

PROTECTION OF HILL LAKES THROUGH EROSION CONTROL WORKS

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ABSTRACT

Soil erosion has a great impact on reservoirs, owing to sedimentation and the degradation of water quality. There are made erosion and sediments effluence differentiation in a watershed with erosion control works and same watershed without erosion control works. The comparative analyze of these tow situation, with erosion control works and same watershed without erosion control works, set of some conclusions.

The erosion is reduced under acceptable limits; a proper cultivation structure mixed with erosion crop system reduced erosion and sediment effluence; a good erosion control works capitalized efficiently rainfall, surface runoff are reduced; an adequate reclamation of outlet network reduces gully erosion; ensemble of land reclamation (cultivation structure, erosion crop system, erosion control works on outlet network) reduces erosion and sediment effluence with 23%.

RESULTS

In the vicinity of Cubul Vulturnilor reservoir there is the watershed Cârjăoani a valley gully. From this watershed about 1872 hectares it was proposed to appropriate an erosion control works, with ought changing the land use (Table 1), showing the effect of these works on the sedimentation process.

-Before reclamation: Crop structure - straw cereals 39 % - cultivator plants 62%; non erosion measure up and down cultivating: the outlet network with ought erosion control works.

-After reclamation: Crop structure - straw cereals 68 % - cultivator plants 24 %, yearly leguminous plants 8%; erosion measure - contour, split and strip farming, banquet terraces; the outlet network (three zone from the upstream to downstream) first zone 7 working (earth dam 4-5 m in height), second zone 6 working (earth dam 5-6 m in height), third zone without working.

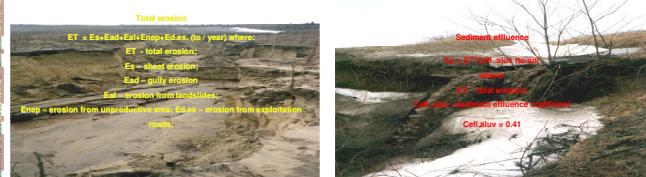
RESEARCH LOCATION

The Cubul Vulturnilor reservoir, located in Eastern Romania in the watershed of the Tutova River, flowing through the Tutova Hills, at 34.5 km from the source, provides a part of the water necessary for the population of Bărad city.

The reservoir was formed along with the erection of an earth dam (17 m in height and 843 m long on crest) with a central weir and a laterally spillway on the right bank. In 1978 it was taken into exploitation, with the following planned characteristics (from Normal Retention Level): available water volume - 9,500,000 m³; dead storage capacity - 300,000 m³; annual sedimentation ratio - 10.000 m³.

According to annual mean sedimentation ratio in this reservoir yearly enter about 221,430 m³ sediments but from the area located in the vicinity of the reservoir enter about 98,755 m³ sediments that mean 65 % from all sediments step in the reservoir in one year. From these volume of sediments that provide from the area located in vicinity of the reservoir 13.1 % provide from the hill slopes and 86.9 % provide from the watersheds.

This value show that the contribution of the watersheds located in vicinity of reservoir direct overflow in the reservoir is the most important quantitative in comparative with the hill slopes.



For erosion calculation, in both cases relationship used it where:
 $Ea = K'S'C'Cs'L*0.3*1.4 (m3/ha)$ where: K - rainfall aggressively, S - soil erodability coefficient, C - crop structure coefficient, Cs - crop cultivating system efficiently coefficient, L - slope length, I - slope land;
 $Ead = Vs*Sad (m3/an)$ where: Vs - sediment volume transported in active sector, Sad - stretched active area;
 $Eal = Eal*Sal$; where: Eal was calculated with USLE equation consider that the surface of landslide like an area with ought vegetation, Sal - stretched active area;
 $Eep = Eep *S*Cs*L*0.3*1.4 (m3/ha)$ where: S - soil erodability coefficient, Cs - crop cultivating system efficiently coefficient, L - slope length, I - slope land;
 $Eup = Eup *Cs*L*0.3*1.4 (m3/ha)$ where: Cs - crop cultivating system efficiently coefficient, L - slope length, I - slope land.

Table 1 Land use and homogeneous calculation area from smallwatershed Cârjăoani						
Land use	Area (ha)		Homogeneous calculation area		(m ²)	
	Before improvement	After improvement	ha	%		
Agriculture	1237.44	66.10	1237.44	66.10	51	
Pastures	302.60	16.16	302.60	16.16	24	
TOTAL agriculture area	1540.04	82.27	1540.04	82.27	75	
Forestry	207.90	11.11	207.90	11.11	27	
Constructions	62.65	3.35	62.65	3.35	1	
Unproductive	81.75	3.38	81.75	3.38	3	
Total	1872.00	100.00	1872.00	100.00	108	

Table 4 Maximum flood discharge on going out section of Cârjăoani watershed									
Flood discharge are calculated of low case and low moments									
Cases: I+Ic and I+Ic+Ib Ib = maximum time of slope flow I = time from beginning of the rain to the end of rain Ic = time when the height of flow on slope is maintained constant									
Time	10	20	30	40	50	60	70	80	
Case	I+Ic	I+Ic	I+Ic	I+Ic	I+Ic	I+Ic	I+Ic	I+Ic	
Moment	I	I+Ib	I	I+Ib	I	I+Ib	I	I+Ib	
Q _{fa}	0.10	4.54	1.00	12.59	2.28	16.64	3.72	19.39	4.62
Q _{fa}	0.05	3.09	0.17	4.04	0.87	9.20	1.23	9.60	1.61

Table 2 Erosion and sediments effluent from Cârjăoani watershed										
Erosion					Sediments effluent					
Erosion form	Before Improvement	After Improvement	Before Improvement							
Sheet erosion	30981	17.5	100	4729	3.8	22	12538	7.2	100	2759
Acute erosions	27362	22.5	100	1008	2.5	25	11300	3.1	100	2295
From pasture	3008	9.3	100	112	3.7	37	1233	4.1	100	456
From forest	11	0.1	100	11	0.1	100	4.4	0.0	100	4.4
From gully erosion	541	8.5	100	324	5.3	60	222	3.6	100	133
From roads	0.3	0.1	100	0.3	0.1	100	0.1	0.0	100	0.0
TOTAL	31123	17.2	100	7054	3.8	33	12760	7.0	100	2892

Height of runoff	W = W ₀ + W ₁	W ₀ = W ₀ (t _c)
t _c = time from beginning of the runoff through the end of rain	W ₁ = W ₁ (t _c)	W ₁ = W ₁ (t _c)
I = time from beginning of the rain to the end of rain	W ₀ = W ₀ (t _c)	W ₁ = W ₁ (t _c)
I _c = time when the height of flow on slope is maintained constant	W ₀ = W ₀ (t _c)	W ₁ = W ₁ (t _c)
W ₀ = runoff volume find in channel at constant moment	W ₁ = runoff volume find in channel at constant moment	
W ₁ = runoff volume who are derived with the equation of continuity		

There are two determination case and from both case there are two characteristic moments
Case Ic: moments I and I+Ib
Case I+Ic: moments Ic and I
where:
t = time from beginning of the runoff through the end of rain
t_c = time when the height of flow on slope is maintained constant
I = time from beginning of the rain to the end of rain
Ic = time when the height of flow on slope is maintained constant

Table 3 Height of runoff from 10% insurance in Cârjăoani watershed									
height (m)	10	20	30	40	50	60	70	80	90
Before improvement	6.60	10.00	11.56	12.50	12.75	12.75	12.25	11.75	10.00
After improvement	5.75	6.50	9.90	9.75	10.00	9.90	9.65	7.00	6.00
Decrease (%)	11.6	35.0	17.4	22.0	25.5	26.6	29.8	30.8	31.2

CONLUSIONS

- The comparative analyze of these tow situation, with erosion control works and same watershed without erosion control works, set of some conclusions:
- The erosion is reduced under acceptable limits (17.2 m³/ha without erosion control works relative to 3.9 m³/ha with erosion control works);
- A proper cultivation structure mixed with erosion crop system reduced erosion and sediment effluence with 20%;
- A good erosion control works capitalized efficiently rainfall, surface runoff are reduced with 11-30%;
- An adequate reclamation of outlet network reduces gully erosion with 60%;
- Ensemble of land reclamation (cultivation structure, erosion crop system, erosion control works on outlet network) reduces erosion and sediment effluence with 23%.

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